

## A note on the foreshock of the 1992 Roermond earthquake, the Netherlands

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Received 30 August 1993; accepted in revised form 15 December 1993

*Key words:* relative location, Roermons earthquake

### Abstract

Vertical components from 12 digital seismic stations which recorded the  $M_L = 5.8$  Roermond earthquake were used to determine the position and magnitude of a foreshock using relative methods. The small shock occurred 0.19 s before and 780 m away from the main shock on its SW-dipping fault plane. The local magnitude of the foreshock is  $M_L = 4.0$ , which corresponds to a seismic moment of  $2.8 \cdot 10^{14}$  Nm and to a seismic energy of  $4.3 \cdot 10^9$  J.

### Introduction

The Roermond earthquake of April 13, 1992, at 01:20 UT with  $M_S = 5.3$  ( $M_L = 5.8$ ) was the largest earthquake in the Lower Rhine Embayment since the 1951 Euskirchen earthquake. Joint hypocenter determination of the main shock and aftershocks using permanent and temporary stations (Camelbeeck et al. 1994) constrains the depth of the main shock to 17 km and allows the identification of the Peel Boundary Fault as the fault responsible for the earthquake. The focal mechanism corresponds to a pure dip-slip dislocation on a fault plane striking  $124^\circ$  and dipping  $68^\circ$  southwestward (Ahorner 1992, Paulssen et al. 1992, Braummiller et al. 1994). The depth of the aftershocks ranges from 10.5 to 20 km.

The purpose of this note is to use arrival time differences and amplitude ratios of P-waves to determine the location and magnitude of a small foreshock of the Roermond earthquake. This foreshock was first identified by Ahorner (pers. comm., April 23, 1992). For the relative location of its hypocenter we used the 'master event' technique and for the relative magnitude determination the ratio of maximum velocities.

### Data analysis

The data used in this study come from the permanent digital seismic stations in Belgium and the Grand-Duchy of Luxemburg, to which we added station Bochum (BUG) of the German Regional Station Network to cover an azimuth gap in the east. The station distribution relative to the main shock epicenter is presented in Fig. 1 and a list of the 12 stations we used is given in Table 1. This 'network' covers about  $180^\circ$  of azimuth, a fact that will render our determinations a reasonable degree of reliability.

The zoomed P-waves of the main shock at these 12 stations show that the main rupture phase was preceded by a small foreshock (Fig. 2). The differences in arrival times were used in a 'master event' analysis in order to determine the relative position (and origin time) of the foreshock with respect to the main rupture phase. When picking the arrival time difference, we also looked at the theoretical travel time curves (Fig. 3). They show that we could expect complications in the 90–100 km epicentral distance interval, where the direct and refracted waves come closely in time. This epicentral distance corresponds approximately to that of stations CLA and BUG and we looked carefully how these two stations were fitted by the data.

The difference  $\Delta t$  at station  $i$  between the arrival times of waves radiated by two events 1 and 2 is given by

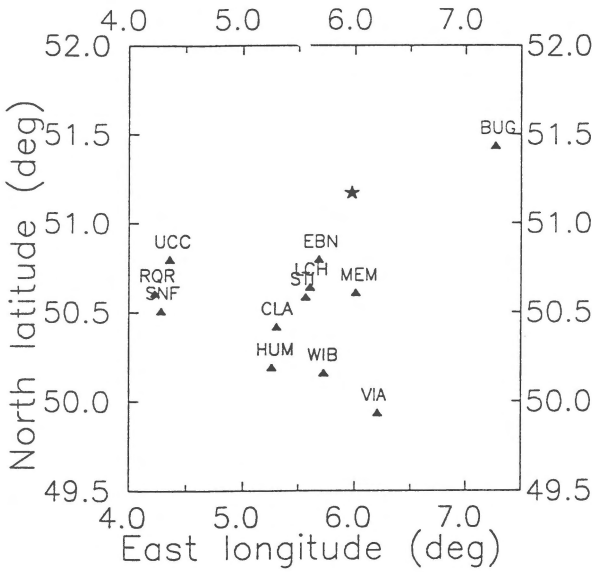


Fig. 1. Location of the 12 stations (▲) listed in Table 1 and the main shock epicenter (★).

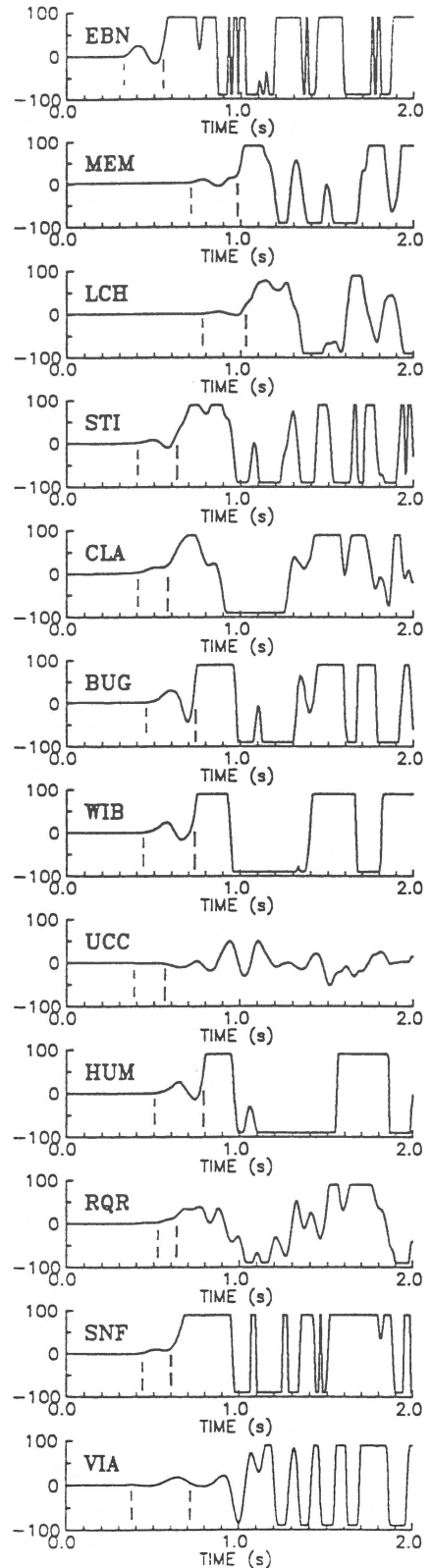
$$\Delta t_i = t_0 - (1/v_h)L\cos\gamma_i, \quad i = 1, \dots, N \quad (1)$$

where  $t_0$  is the difference in origin times,  $L$  is the distance between the foci 1 and 2,  $v_h$  is the wave velocity in the focal region (in our application of P-waves at 17 km depth),  $\gamma_i$  is the angle between the ray leaving focus 1 and the direction connecting the two foci, and  $N$  the number of stations. Equation (1) is valid as long as the distances between the focal region and stations are much greater than distance  $L$ . In order to overcome the non-linearity of Equation (1) we conveniently re-write  $L\cos\gamma_i$  as the scalar product of the vector  $\mathbf{L}$  (starting in focus 1 and ending up in focus 2) with the unit vector  $\mathbf{e}_i$  pointing in the ray-leaving direction. Thus, for  $N = 12$  we find an overdetermined linear system of 12 equations

$$\Delta t_i = t_0 - (l/v_h) \sum_{k=1}^3 L_k e_{ik} \quad i = 1, \dots, 12 \quad (2)$$

→

Fig. 2. P-wave trains in increasing order of epicentral distance displaying the foreshock signature. The units for the vertical axes are  $\mu\text{m/s}$ . Dashed lines mark the arrival time difference between foreshock and main shock. Data were clipped artificially except for those from stations EBN, CLA and SNF. For station codes and location see Table 1 and Fig. 1.



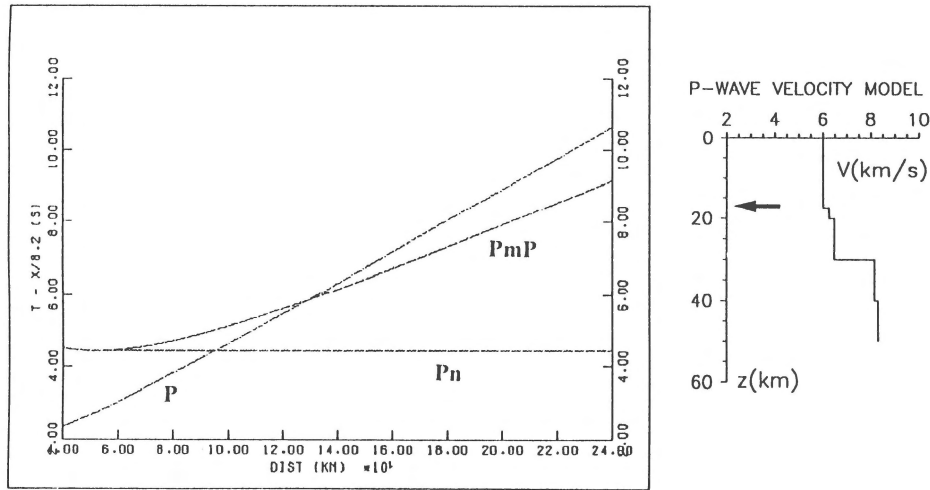


Fig. 3. Theoretical travel time curves (left) for the velocity model given at the right, depicting the direct wave (P), Moho-reflected wave (PmP) and Moho-refracted wave (Pn) branches. The arrow in the velocity model indicates the depth of the focus.

Table 1. List of stations used in the master event location analysis and magnitude determination for the foreshock of the 1992 Roermond earthquake

Station	Epicentral distance (km)	Azimuth $\alpha$ ( $^{\circ}$ )	Take-off angle $\Theta$ ( $^{\circ}$ )	Time difference $\Delta t$ (s)	Ratio of maximum ground velocities
EBN	46	203	110	0.224	12.7
MEM	64	176	105	0.240	15.5
LCH	65	202	105	0.248	13.4
STI	71	202	103	0.224	13.1
CLA	96	208	68	0.200	6.2
BUG	97	72	68	0.262	19.3
WIB	114	188	47	0.264	17.5
UCC	119	249	47	0.152	3.0
HUM	120	204	47	0.240	14.8
RQR	137	242	47	0.144	17.4
SNF	139	238	47	0.184	14.2
VIA	140	172	47	0.272	62.0

with 4 unknowns, i.e.  $t_0$ ,  $L_1$ ,  $L_2$  and  $L_3$ .  $L_k$  are the vector components of  $\mathbf{L}$  indicating the relative distances along NS, EW and downward axes. The components of  $\mathbf{e}_i$  are given by  $e_{i1} = \sin\Theta_i \cos\alpha_i$ ,  $e_{i2} = \sin\Theta_i \sin\alpha_i$  and  $e_{i3} = \cos\Theta_i$ , where  $\Theta_i$  is the take-off angle and  $\alpha_i$  is the azimuth as listed in Table 2. We used  $v_h = 6$  km/s. Equation 2 was solved using a classical least-

Table 2. Hypocenter and source parameters of the foreshock as determined from the reference parameters of the main shock adopted after Braunmiller et al. (1994) and Camelbeeck et al. (1994)

Parameters	Main shock	Foreshock
Origin time (UT)	01:20:03.10	01:20:02.91 $\pm$ 0.02
Latitude ( $^{\circ}$ N)	51.170	51.174 $\pm$ 0.13 km
Longitude ( $^{\circ}$ E)	5.970	5.961 $\pm$ 0.09 km
Depth (km)	17.0	16.9 $\pm$ 0.1
Seismic moment $M_0$ (Nm)	8.3.10 <sup>16</sup>	(2.8 $\pm$ 1.1).10 <sup>14</sup>
Local magnitude $M_L$	5.8	4.0 $\pm$ 0.4
Source radius $r$ (km)	2.1	0.5 $\pm$ 0.1
Brune stress drop $\Delta\sigma$ (MPa)	4.1	1.3 (tentatively)

squares approach and the standard errors of the four unknowns were propagated to all derived results. Figure 4 displays the obtained linear dependence between  $\Delta t_i$  and  $\cos\gamma_i$  according to Equation 1. The observations at stations CLA and BUG do not deviate from the trend of the data and do not change the results when removed.

From the components  $L_k$  we then computed the distance between the two foci,  $L = (L_1^2 + L_2^2 + L_3^2)^{1/2}$ , then the azimuth  $\phi$  and the dip  $\delta$  of foreshock position relative to the mainshock hypocenter are:  $\phi = \arctan(L_2/L_1)$  respectively  $\delta = \arccos(L_3/L)$ . The foreshock occurred  $0.19 \pm 0.02$  s before the main shock at a distance  $L = 780 \pm 110$  m in a direction given by an

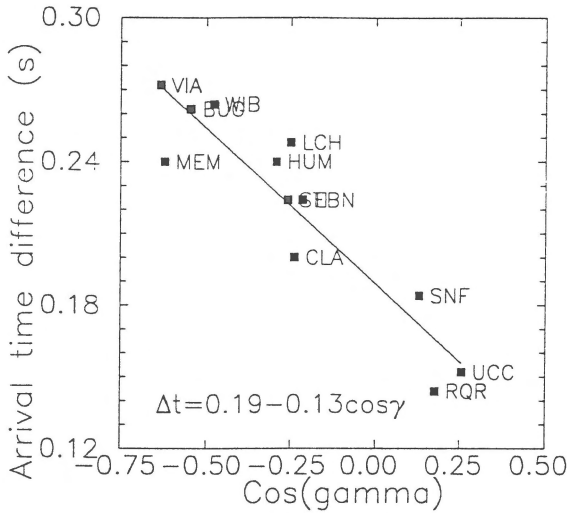


Fig. 4. The measured arrival time differences  $\Delta t_i$  (■) are a function of  $\cos \gamma_i$  and the obtained linear fit (line) according to the method described in the text. For station codes and location see Table 1 and Fig. 1.

azimuth of  $310^\circ \pm 9^\circ$  and a dip of  $-8^\circ \pm 7^\circ$  (a negative dip means above the local horizon). Vector **L** indicating the position of the foreshock is presented in Fig. 5 on the fault-plane solution of Ahorner (1992). The foreshock is situated on the SW-dipping nodal plane, offering an unambiguous identification of the actual rupture plane. The same choice was made from seismotectonic reasons by Ahorner (1992) and Pelzing (1992) and from aftershock distribution by Camelbeek et al. (1994).

To infer the magnitude of the foreshock we applied also a relative method. We measured the ratio of maximum ground velocities  $V_2/V_1$  from the vertical component P-wave trains, where the indices 1 and 2 refer to the foreshock and main shock, respectively. Then, for a magnitude scale of the form  $M_L = \log A + b$ , where  $A$  is the maximum ground displacement usually within the S-wave train, and assuming that the S-wave amplitude ratio equals the P-wave amplitude ratio (the same focal mechanism for both shocks), we find:

$$M_{L2} - M_{L1} = \log(V_2/V_1) + \log(f_1/f_2) \quad (3)$$

Here we used that  $A = V/2\pi f$ , where  $f$  is the predominant frequency in the signal. We adopted a value  $f_2 = 1$  Hz for the main shock (Ahorner 1992, Braunmiller et al. 1992) and  $f_1 = 4.5$  Hz for the foreshock as the inverse of the mean 'time difference' in Table 1.

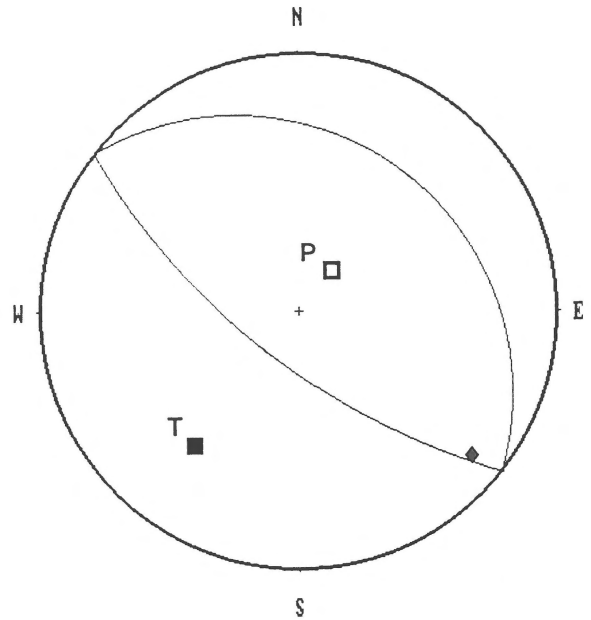


Fig. 5. Vector **L** (◆) indicating the position of the foreshock on the fault-plane solution for the main shock as obtained by Ahorner (1992). Stereographic projection on the lower hemisphere. P: compressional axis, T: tensional axis.

In the magnitude determination, we rejected station VIA due to its strong site response (Oncescu et al. 1994). The average ratio of maximum ground velocities was  $15.3 \pm 2.2$ , resulting in a magnitude difference of  $1.8 \pm 0.2$  units. Consequently, with  $M_{L2} = 5.8$  (Camelbeek et al. 1994) we find  $M_{L1} = 4.0 \pm 0.2$  (or  $\pm 0.3$  if one takes  $M_{L2} = 5.8 \pm 0.2$ ). We believe that an estimate of  $f_1$  may range between 3.5 and 6 Hz, i.e. an error factor of 1.3. Considering also this uncertainty we finally arrive at a magnitude estimate of  $M_{L1} = 4.0 \pm 0.4$ . So, the foreshock is larger than the largest aftershock!

Extrapolating the empirical relationships obtained by Oncescu et al. (1994),  $\log M_0$  (Nm) =  $1.02 M_L + 10.36$  and  $\log E_s$  (J) =  $1.90 M_L - 17.8$  for exactly the same region but for the magnitude interval  $M_L = 1.9$ – $3.4$ , we arrive at an estimate of the seismic moment  $M_0 = 2.8 \cdot 10^{14}$  Nm and the released seismic energy  $E_s = 4.3 \cdot 10^9$  J for the foreshock. If we further adopt the predominant frequency  $f_1 = 4.5$  Hz as the P wave corner frequency of the foreshock, we obtain an estimate for its source radius,  $r_1$ , and stress drop,  $\Delta\sigma_1$ , relative to the main shock using the relations:

$$r_1/r_2 = f_{c2}/f_{c1} \text{ and } \Delta\sigma_1/\Delta\sigma_2 = (M_{01}/M_{02})(r_2/r_1)^3 \quad (4)$$

From the main shock source parameters (Braunmiller et al. 1992) we obtain the results given in Table 2. The standard error of  $\Delta\sigma$  was not determined due to the very strong dependence on radius, i.e.  $f_1$  estimate. Therefore  $\Delta\sigma$ , should be considered with caution.

### Final remarks

The determined foreshock position further corroborates the rupture plane as being the one dipping  $68^\circ$  southwestward. One may speculate that the main rupture phase started on the same fault plane, but at the margin of the foreshock rupture zone, as the relative distance of  $780 \pm 110$  m is comparable with the foreshock source radius of about 500 m. The foreshock magnitude is approximately two units smaller than the main shock magnitude.

### Acknowledgements

We thank K. Bonjer and R. Verbeiren for encouraging this study and for critically reading the manuscript. Two anonymous reviewers helped with their comments. We also thank T. van Eck for accepting a late contribution. This study has been supported by the German Research Association (SFB 108), by the IDNDR Project of the University of Karlsruhe and by the Royal Observatory of Belgium.

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